Using a set of equations (Newton-Euler equations with four variables: position of the insect, horizontal and vertical velocity and angular velocity) there is a simulation of a longitudinal flight considering forces from wing flapping. Data were taken from experiments and they were fitted into Fourier series until the eight harmonic order. These forces consider the effect at different velocities of the air and also at different angles of attack. After that, a first simulation includes the zero order harmonics which is going to be a model nonlinear time invariant, in this simulation is seen the effect of perturbing the initial condition of the horizontal velocity. In the following set of plots are considering the Fourier series until the eight order harmonics in order to show the effect of two different initial time conditions. Finally, for the nonlinear time invariant system there is a 3D plot showing how the position of the insect is changing with reference to the other three variables considered in the system.
Introduction

Many investigations have been done to analyze stability of aircraft which has been explored from different approaches. These approaches can be split in three ways: the first one based in experiments commonly cited as flow visualization and the second one based in theoretical frame usually called computer fluid dynamics. Flow visualization requires of using complex and well-designed set up in order to recover appropriate information while computer fluids dynamics requires of representative values in the coefficients which are part of the equations to simulate the system. In both ways a strong background is required and also an adequate interpretation of results would be important. However, there is an alternative approach which is simplified in terms of application and also with wide versatility. This third approach is called aircraft stability which in general follows a framework similar to the one used to study airplanes or helicopters stability.

Adapting aircraft stability to the flight of insects should be made since insects can fly by means of forces produced in the wings flapping. This implies that insects follow a particular kinematics. But, in this work what matters from wings are the total force and/or moment produced [1].

Although, any insect follows similar characteristics or patterns, it is easily observed that size, shape, weight and others are sufficiently different to be impossible achieve a representative and general model. Under this situation have better been explored possibilities to simulate a flight of a locust [2]. But, in the first part develops a methodology to log a set of data from experiments which are going to be used in a set of equations to reproduce a flight under a linearized model.
This set of data rather consider some properties as size, weight, moment of inertia, forces produced because of the flapping, among others.

Main characteristics of the locust

As the model is determined by physical properties of the locust, then it is important to cite some of them. For example, to have an idea the wing beat frequencies of the largest butterflies is around (c. 40 rad/s in the 1 × 10−3 kg birdwing Troides rhadamantus3) which is comparable to the rotor frequencies of the smallest helicopters (44 rad/s in the 2×103 kg Eurocopter Bo1054) [3].

The desert locust is a robust, migratory, four-winged insect of 0.1m span, optimized for endurance, rather than maneuverability, and with a range of several kilometers at its cruise speed of 4 m/s. Although locusts do not vary in overall body plan, different individuals vary markedly in size. The wings beat at c. 20 Hz, with the hindwing leading the forewing by $\pi/6$ rad. The hindwing typically sweeps 110° through every half-stroke, while the forewing sweeps through 70°. The hindwing comprises a collapsible fan consisting of a flexible membrane with supporting ribs radiating from the root. Each wing is moved by 10 muscles, and with no separate control surfaces, flight control is made by changes in the wing kinematics. Slower flight control is made by moving the legs and abdomen, which act as a rudder and also shift the center of mass. Locusts are equipped with a range of sensors known to be used in correctional flight control. The antennae sense airspeed, analogous to a Pitot tube. Wind-sensitive hairs on the head sense aerodynamic incidence. Each wing has at its base strain receptors involved in flight control that
may measure total wing loading, but perhaps more likely monitor wing kinematics: they have no direct or functional analog in conventional aircraft [3].

From observations of biologists it is pointed out that compound eyes works as horizon detectors measuring bank and pitch angle, and as optic flow detectors measuring heading and perhaps pitch, roll and yaw rate. Additionally, locusts are not known to have any sense of gravity in flight. Although vision is certainly important in insect flight control, it cannot give absolute measurements of bank and pitch angle unless referenced to gravity, and is ambiguous in respect of certain aspects of self-motion [3].

**Newton-Euler Equations**

To simulate the flight, this framework is going to be based in the set of equations called Newton-Euler equations which are showed below:

\[
\begin{align*}
\dot{u} &= -wq + \frac{X}{m} - g \sin \theta \\
\dot{w} &= uq + \frac{Z}{m} + g \cos \theta \\
\dot{q} &= \frac{M}{I_{yy}} \\
\dot{\theta} &= q
\end{align*}
\] (1)

From this set of equations is important to say that simulation is going to consider a 2D simulation flight which is going to be longitudinal with respect to the insect. Formally, \(u\) and \(w\) are the velocity with respect to the horizontal and vertical axis correspondingly, \(q\) means the
angular velocity with respect to the center of mass of the insect and \( \theta \) is the angle with respect to the horizontal axis. This can be better explained in the Figure 1 showed below:

![Diagram of insect with axes labeled](image)

Fig.1 Variables considered in the model.

**Experiments**

There were several concerns regarding to data obtained from experiments. Basically, attending needs of the Newton-Euler equations some values as the weight, moment of inertia and forces should be as accurate as possible. Considering three types of locusts some data were considered in the simulation and that information can be summarized in Table 1 [1].

<table>
<thead>
<tr>
<th>Locust</th>
<th>Reference body mass (g)</th>
<th>Reference body length (mm)</th>
<th>Moment of inertia Iyy (10^-9 kg/m²)</th>
</tr>
</thead>
<tbody>
<tr>
<td>“R”</td>
<td>1.8490</td>
<td>46.0</td>
<td>232.8</td>
</tr>
<tr>
<td>“G”</td>
<td>1.4357</td>
<td>40.5</td>
<td>140.3</td>
</tr>
<tr>
<td>“B”</td>
<td>1.8610</td>
<td>46.0</td>
<td>236.0</td>
</tr>
</tbody>
</table>
Although, in Table 1 considers three type of locust, in this midterm progress report is considered a simulation for the locust type “R”.

**Logging forces**

Logging forces is important since they are going to be the reference in the simulation. As the main goal of this work is analyze stability and forces plays an important role in the model; a brief explanation of the experiments is mentioned. Essentially, a locust was attached to the top of a needle. That locust was inside of a wind tunnel (see Fig. 2) and the forces were recorded at different wind speeds and also at different position of the insect (angle with respect to the horizontal axis). Forces recorded were recorded in an interval from 2 to 5.5m/s and also at angles from 0° to 14°; these ranges were given from observations when the locust is found in a free flight [1]. At this stage, it is expected to have a reaction of the locust as in a real free flight, however, a locust might recognize that is not a real flight but rather a reaction to move away of a “risky situation”; then forces might not be represented accurately.

**Results**

Once forces were recorded, it was needed to preprocess data. This preprocess implies that was done a simplification of forces variability to one representative flapping. This means that there is an assumption that flapping is uniform during the flight and one period of flapping is going to be exactly equal to the next one; which it does not occur in a real flight but it reduces the set of data significantly. Then, data obtained from experiments can be visualized in Fig 3, (left plot) where variability of forces for one cycle of flapping (X correspond to the horizontal direction) at different angles of the locust (from 0° to 14°).
Fig. 2 Recording forces from a locust.

Fig 3 (left plot) includes thousands of points and the set of data may not be easy to handle. To overcome this situation was used Fourier series. Fourier series helps a lot since the set of data was reduced to a few coefficients which are able to reproduce original data with an acceptable approximation, as it is seen in the Fig 3 (right plot). Once again, data is compacted to a set of coefficients to be used in Fourier series. The maximum order of the harmonics is eight and it is good enough to have high accuracy in the representation of the original set of data.

Fig 3 Forces obtained from experiments.
Fourier series can be represented by the equation (2) and it was used for the force $X$ in the horizontal direction, the force $Z$ in the vertical direction and the moment $M$ at the center of mass of the insect.

$$P(t) = \sum_{n=0}^{b} (a_n \cos n\omega t + b_n \sin n\omega t)$$

As the first task was reproduced force $X$ at different positions of the locust for one cycle of flapping. Results are showed in the Fig 4 (left plot), while results obtained in the paper are showed in Fig 4 (right plot). In the same way was done for the force $X$ at different wind speeds also for one cycle of flapping as it is showed in Fig 5.

Forces in the vertical direction were reproduced at different angles and different wind speeds. In the same way for the moment as it is seen Fig. 6; where right plots corresponds to original plots and left plots corresponds to the ones reproduced.

Fig 4. Reproducing $X$ force at different angles of the locust for one cycle of flapping.
Fig 5. X force at different wind speeds for one cycle of flapping.

Fig 6. Vertical force Z and moment M at different angles of the locust and different wind speeds.
Forces and moment showed previously follows equations (3):

\[
X(\alpha, U, t) = \sum_{n=0}^{8} (a_{1,n} \cos n \omega t + b_{1,n} \sin n \omega t) + (\alpha - \alpha_{ref}) \sum_{n=0}^{8} (a_{2,n} \cos n \omega t + b_{2,n} \sin n \omega t) + U - U_{ref} n=08(a_{3,n} \cos n \omega t + b_{3,n} \sin n \omega t)
\]

\[
Z(\alpha, U, t) = \sum_{n=0}^{8} (a_{1,n} \cos n \omega t + b_{1,n} \sin n \omega t) + (\alpha - \alpha_{ref}) \sum_{n=0}^{8} (a_{2,n} \cos n \omega t + b_{2,n} \sin n \omega t) + U - U_{ref} n=08(a_{3,n} \cos n \omega t + b_{3,n} \sin n \omega t)
\]

\[
M(\alpha, U, t) = \sum_{n=0}^{8} (a_{1,n} \cos n \omega t + b_{1,n} \sin n \omega t) + (\alpha - \alpha_{ref}) \sum_{n=0}^{8} (a_{2,n} \cos n \omega t + b_{2,n} \sin n \omega t) + U - U_{ref} n=08(a_{3,n} \cos n \omega t + b_{3,n} \sin n \omega t)
\]

which in general are similar and follows the equation (4).

\[
P(\alpha, U, t) = P_{ref}(t) + P_{\alpha}(t)(\alpha - \alpha_{ref}) + P_{U}(t)(U - U_{ref})
\]

The equation mentioned before represents how the forces and moment can be handled once they fitted in Fourier series; and basically considers that a force or moment have a reference which is going to be affected by the position of the locust and also by the velocity of the locust. For example for the horizontal force X can be represented as equation (5).

\[
X(\alpha, U, t) = X_{ref}(t) + X_{\alpha}(t)(\alpha - \alpha_{ref}) + X_{U}(t)(U - U_{ref})
\]

But P involves terms cited in equation (6)

\[
P = [X, Z, M]
\]
Now connecting forces and moment in the Fourier series, then the set of Newton-Euler equations will be equation (7).

\[
\begin{align*}
\dot{u} &= -wq + \frac{X_{\text{ref}}(t)}{m} + \frac{X_{\alpha}(t)}{m} \left( \tan^{-1} \frac{w}{u} - \alpha_{\text{ref}} \right) \\
&\quad + \frac{X_U(t)}{m} \left( \frac{\sqrt{u^2 + w^2}}{u} - U_{\text{ref}} \right) - g \sin \theta \\
\dot{w} &= uq + \frac{Z_{\text{ref}}(t)}{m} + \frac{Z_{\alpha}(t)}{m} \left( \tan^{-1} \frac{w}{u} - \alpha_{\text{ref}} \right) + \frac{Z_U(t)}{m} \left( \frac{\sqrt{u^2 + w^2}}{u} - U_{\text{ref}} \right) \\
&\quad + g \cos \theta \\
\dot{\alpha} &= \frac{M_{\text{ref}}(t)}{I_{yy}} + \frac{M_{\alpha}(t)}{I_{yy}} \left( \tan^{-1} \frac{w}{u} - \alpha_{\text{ref}} \right) + \frac{M_U(t)}{I_{yy}} \left( \frac{\sqrt{u^2 + w^2}}{u} - U_{\text{ref}} \right) \\
\dot{\theta} &= q
\end{align*}
\]

With this new set of equations was looked for the quasi-static equilibrium in order to start simulations from those values. It is said that is quasi-static because the equations are set equal to zero in the left hand side, then specific values are found for every one of the four variables, but velocity in the vertical and horizontal are different from zero. This non zero value for the velocity variables means that the insect has an equilibrium during the flight considering this set of equations. Values found and used for the simulation are showed in Table 2.

Table 2. Conditions for quasi-static equilibrium of each locust.

<table>
<thead>
<tr>
<th>Locust</th>
<th>( \theta ) (deg)</th>
<th>( \alpha ) (deg)</th>
<th>U(m/s)</th>
</tr>
</thead>
<tbody>
<tr>
<td>“R”</td>
<td>26</td>
<td>6</td>
<td>4.48</td>
</tr>
<tr>
<td>“G”</td>
<td>5</td>
<td>12</td>
<td>2.93</td>
</tr>
<tr>
<td>“B”</td>
<td>23</td>
<td>9</td>
<td>4.79</td>
</tr>
</tbody>
</table>

Quasi-static equilibrium estimation is coming from equations (1) which will be used as the initial conditions. Reproducing for locust type “R”, velocity \( u \) is equal to 4.48*cos(6); velocity \( w \) is equal to 4.48*sin(6), \( q \) is equal to zero and \( \theta = 26/57.29 \) (converted to radians). In this stage is
important to indicate that $\alpha$ is the angle formed of the speed vector (U) with respect to the horizontal axis. With these initial conditions is showed a first simulation which considers a Fourier series for forces and moment with order zero which corresponds to a nonlinear model time invariant; in other words, implies that forces or moment during one cycle of flapping are constant. Results are showed in Fig. 7. Plots in the right side correspond to the ones from the paper while plots in the left side correspond to the ones reproduced using Matlab.

![Fig 7. Simulation for a Non linear time invariant model with perturbation in the u-velocity.](image)

In Fig. 7 there is a perturbation for the initial condition corresponding to u velocity by a value of 0.002m/s to see if the model is stable; getting similar plots as in the paper; from here it is possible to see how drastically the curve change with such a small perturbation. However, reproduction of these plots accomplishes the idea of potential instability. This instability could be explained because of the averaged force for every flapping.
Since it is possible to simulate a flight considering until the eight order of harmonics in Fourier series, which covers information of variability of forces or moment during one cycle of flapping. It will be showed now in Fig. 8 results for a model called nonlinear time periodic model. In this case, initial conditions are set equal to the quasi-static equilibrium but initial time is altered for 0.025s; a value equivalent to a half cycle of flapping. This perturbation accomplishes the idea of how much would change a possible trajectory of the flight because starting of flapping with open wings instead of closed wings (when initial time is equal to zero). Again, instability of the system is present. As the model has used all the information from experiments; some conclusions come up. For instance, the model is still weak to show simulation of an insect flight, several reasons are valid as data are not representative of a free flight, methodology to obtain data can be improved and the framework used does not represent the phenomena under analysis.

Fig 8. Simulation of a nonlinear time periodic model with perturbation in the initial time.
Finally, it is showed a last figure (Fig. 9) which correspond a phase portrait for the variable $\theta$. This plot is in 3D to give a better picture of how $\theta$ is changing with respect to the other three variables. It is expected in this figure to have a constant smooth change in values of $\theta$ because this behavior can be interpreted that the model is potentially stable. However, it is easy to see that there are two points where $\theta$ changes abruptly implying that the model cannot be useful to manipulate a flight; in other words, trajectories wanted might be restricted at certain zones or domain.

**Conclusions**

Since the model is based in forces recorded, it is suspicious that forces do not represent a real free flight. This is possible since several factors were limiting it; for instance, forces were not accurate because of the instruments used, the insect can have different reactions under this “altered conditions” to simulate the flight. Additionally, some assumptions were made as the
gravity, weight and moment of inertia are constant which is not true and it is easily noticed in the moment of inertia because of the flapping.

Additionally, when the experiments were performed, there was a recording of forces in open loop. Under this situation, it is assumed that the insect does not control the flight, which is not true. Then forces to manipulate the flight might already be included in the set of data given in the paper however so far it is not possible to obtain those forces apart.

**Future work**

In first place, it will be considered the other two types of locust in order to have a complete reproduction of results from the paper. But additionally, it will be explored possibilities to have a stable flight, which means to be able to manipulate the flight. Based in the Fourier series as the source of forces, the goal is to find the right coefficients in order to simulate for longer time a stable flight.

**References**

